



UNIVERSITY *of* LIMERICK  
OLLSCOIL LUIMNIGH

Faculty of Science and Engineering

**END OF SEMESTER ASSESSMENT PAPER**

MODULE CODE: MA4607

SEMESTER: Autumn 2012-13

MODULE TITLE: Introduction to Fluids

DURATION OF EXAMINATION: 2 1/2 hours

LECTURER: Prof. S. O'Brien

PERCENTAGE OF TOTAL MARKS: 90%

EXTERNAL EXAMINER: Prof. T. Myers

**INSTRUCTIONS TO CANDIDATES: Full marks for 5 questions. There are some useful results at the end of the paper.**

### 1 Streamlines, conservation of mass, rates of change

- (a) A glider, drifting at the local air velocity  $\mathbf{u}$ , is measuring  $c(x, y, z, t)$ , the concentration of a pollutant in the air. What is meant by the ordinary partial derivative  $\frac{\partial C}{\partial t}$  and the convective rate of change  $\frac{DC}{Dt}$ ? Use the chain rule to *prove* that

$$\frac{DC}{Dt} = \frac{\partial C}{\partial t} + \mathbf{u} \cdot (\nabla C).$$

If, instead of drifting, the velocity of the glider is  $\mathbf{v}$ , what derivative measures the rate of change of pollutant as measured from the glider?

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- (b) The velocity vector for a particular flow  $\mathbf{u}(x, y, z, t) = (u, v, w)$  has been calculated for all values of  $x, y, z, t$ . Explain what is meant by the streamlines of the flow and show that at any particular time they are given by:  $\frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w}$ .

Sketch the streamlines (with direction arrows) for the flow

$$u = \alpha x, v = -\alpha y, w = 0,$$

where  $\alpha$  is a positive constant. Let the concentration of some pollutant in the fluid be

$$c(x, y, t) = \beta x^2 y e^{-\alpha t},$$

for  $y > 0$ , where  $\beta$  is a constant. Does the pollutant concentration following a fluid element change with time?

Sketch the velocity profile for the shear flow  $\mathbf{u} = (3y, 0, 0)$ ,  $0 \leq y \leq 1$ .

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- (c) Using the principle of conservation of mass and the divergence theorem, derive the continuity equation:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$

in the usual notation. If the flow is incompressible, deduce that  $\nabla \cdot \mathbf{u} = 0$ .

Under what conditions does the velocity field

$$\mathbf{u} = (a_1 x + b_1 y + c_1 z)\mathbf{i} + (a_2 x + b_2 y + c_2 z)\mathbf{j} + (a_3 x + b_3 y + c_3 z)\mathbf{k}$$

represent an incompressible flow where  $a_i, b_i, c_i$  are constants?

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## 2 Vorticity, Bernoulli

- (a) Define vorticity. For a two dimensional flow  $\mathbf{u} = (u(x, y, t), v(x, y, t), 0)$ , show that the vorticity is given by  $(0, 0, v_x - u_y)$ . Discuss briefly how vorticity is created in viscous flows.

A body of fluid is in rigid rotation with velocity vector  $\mathbf{u} = (-\Omega y, -\Omega x, 0)$  where  $\Omega$  is a constant. Compute the vorticity and comment on your result.

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- (b) Beginning with the Euler equations in the form:

$$\frac{\partial \mathbf{u}}{\partial t} + (\nabla \times \mathbf{u}) \times \mathbf{u} = -\nabla H; \quad H \equiv p/\rho + \frac{1}{2} \mathbf{u}^2 + \chi,$$

prove the following theorems:

- (i) the Bernoulli streamline theorem that if an ideal fluid is in steady flow, then  $H$  is constant along a streamline,  
 (ii) the second Bernoulli theorem that if an ideal fluid is in steady *irrotational* flow then  $H$  is constant throughout the whole flow field,  
 (iii) the vorticity equation for ideal flow in the form:

$$\frac{D\boldsymbol{\omega}}{Dt} = (\boldsymbol{\omega} \cdot \nabla) \mathbf{u},$$

- (iv) the vorticity equation for two dimensional ideal flow:

$$\frac{D\omega}{Dt} = 0.$$

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## 3 Non-dimensionalisation

- (a) Starting with the two dimensional steady Navier-Stokes equations, non-dimensionalise velocities, distances and the pressure using the scales  $L, U, \rho U^2$  and demonstrate the occurrence of a Reynolds number  $R \equiv UL/\nu$ . Explain the physical significance of the Reynolds' number. What approximations might you make if

- (i)  $R \gg 1$ ,  
 (ii)  $R \ll 1$ .

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- (b) Prove that for flow at small Reynolds number (Stokes flow)

$$\mathbf{0} = -\nabla p + \mu \nabla^2 \mathbf{u}$$

with boundary condition  $\mathbf{u} = \mathbf{f}_b(\mathbf{r})$ , the flow is reversible.

Deduce that a small sphere moving parallel to a wall in Stokes flow will experience no force in the direction parallel to the wall.

Describe an experiment (involving a mechanical fish, for example) to verify the reversibility property.

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- (c) A two dimensional flow with velocity vector  $\mathbf{u} = (u(x, y), v(x, y), 0)$  in  $y \geq 0$  occurs in the vicinity of a stationary wall located along the  $x$  axis  $y = 0$ . Name the simplest equations of motion suitable for the flow (Euler or Navier-Stokes) and the boundary conditions for  $u$  and  $v$  on  $y = 0$  if

- (i) the liquid is inviscid.  
 (ii) the liquid is viscous.

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#### 4 Problems involving the Navier-Stokes equations

- (a) Viscous fluid flows between two stationary rigid boundaries  $y = \pm h$  under a constant known pressure gradient  $P = -dp/dx$  i.e.,  $\nabla p = (-P, 0, 0)$ . Show that the Navier-Stokes equations reduce to a single ordinary differential equation for  $\mathbf{u} = (u(y), 0, 0)$  and that

$$u = \frac{P}{2\mu}(h^2 - y^2), v = w = 0.$$

9 %

- (b) An incompressible fluid, with kinematic viscosity  $\nu$  and uniform density  $\rho$ , is restricted to the region between the planes  $y = 0$  and  $y = b$ . The fluid motion is steady and the velocity vector takes the form  $\mathbf{u} = U(y)\mathbf{i} + V_0\mathbf{j}$  where  $V_0$  is a constant.

There are no body forces and the pressure gradient is specified to take the value  $\nabla p = (-G, 0)$  throughout the fluid, where  $G$  is a positive constant.

Show that  $U(y)$  satisfies the equation:

$$\frac{d^2U}{dy^2} - \frac{V_0}{\nu} \frac{dU}{dy} = -\frac{G}{\rho\nu}.$$

If there is no slip imposed at  $y = 0$  and  $y = b$ , solve the ordinary differential equation to find  $U(y)$ .

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### 5 Navier-Stokes equations and stress tensor

- (a) Explain what is meant by the stress vector with typical component  $v_i$  and the stress tensor with typical component  $T_{ij}$ . *Explain* the significance of the relationship  $v_i = T_{ij}n_j$ .  
For the two dimensional flow  $\mathbf{u} = (y^2, 0, 0)$ ,  $p = 2\rho\nu x$ , calculate the stress tensor at any point in the flow and the stress vector on an infinitesimal element located at  $(1, 0, 0)$  with unit normal  $(0, 1, 0)$ . 6 %
- (b) *Derive* Cauchy's equation of motion (see page 7) for a deforming continuous medium. (A statement of the tensor divergence theorem is given on the last page). 6 %
- (c) Using Cauchy's equation of motion and the constitutive relation for a Newtonian viscous fluid (see page 7), *derive* the Navier-Stokes equations. 6 %

### 6 Thin film approximation

- (a) Starting with the two dimensional steady Navier-Stokes equations, with a velocity field of the form  $\mathbf{u} = (u, 0, w)$  (using  $U$  as the main velocity scale and  $\frac{\mu UL}{H^2}$  as the pressure scale) derive the *thin film approximation*:

$$\frac{\partial p}{\partial x} = \mu \frac{\partial^2 u}{\partial z^2}, \quad \frac{\partial p}{\partial z} = 0, \quad \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

assuming that the length scales are  $L, H$  with  $H \ll L$ . 9 %

- (b) A thin splash of honey on a window pane (with known liquid properties  $\mu, \rho, \nu$ ) has an initial configuration given by  $z = h(x, 0) = f(x)$  where  $f(x)$  is a known function defined on  $-\infty < x < \infty$ . The honey trickles under gravity down the window pane (with the  $x$  direction pointing downwards). Assume the problem is uniform in the  $y$  direction ( $\partial/\partial y = 0$ ) and that the air next to the free surface exerts zero shear stress ( $\mu \frac{\partial u}{\partial z} = 0$ ) and zero pressure on the liquid film.
- *Formulate* the problem modelling the flow in the film of honey, writing down the governing equations and all the relevant boundary conditions. *Assume first that the free surface described by  $z = h(x, t)$  is known.* Solve this problem for  $\mathbf{u} = (u, 0, w)$  and the pressure  $p(x, z, t)$  using the thin film approximation.
  - If the free surface of the honey film is described by  $z = h(x, t)$  then explain why  $D/Dt(z - h(x, t)) = 0$  on  $z = h(x, t)$  for all time. If for a particular flow  $\mathbf{u} = (u, 0, w)$  show that the above

so-called “kinematic” condition reduces to:  $h_t + uh_x = w$  on  $z = h(x, t)$ .

Hence write down an evolution equation for the free surface  $h(x, t)$ .

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7 Answer any 2 of the following:

- (a) Consider two parallel plane walls of length  $2a$  ( $-a \leq x \leq a$ ), of infinite extent in the  $y$  direction, which are separated by a thin film of viscous liquid with one of the walls moving away from the other at speed  $dh/dt$  where  $z = h(t)$  is the separation at any time. Assuming that the velocity field takes the form:

$$\mathbf{u} = (u(x, z, t), 0, w(x, z, t)),$$

use the thin film approximation of 6(a) to find the velocity and show that  $p = \frac{6\mu}{h^3} \frac{dh}{dt} (x^2 - a^2)$ . Deduce that the force per unit length in the  $y$  direction required to maintain the motion is:

$$F = \frac{8\mu a^3}{h^3} \frac{dh}{dt}.$$

You may assume that the pressure at  $x = \pm a$  is zero. What is the significance of  $F \sim O(h^{-3})$  as  $h \rightarrow 0$ ?

- (b) Explain briefly what is meant by the continuum hypothesis. At a recent numerical analysis conference, there was much discussion when one author, while modelling a fluid flow problem, used finite differences to approximate the governing Navier-Stokes equations. For example he took:

$$\frac{\partial p}{\partial x} = \frac{p(x+h, y, z, t) - p(x, y, z, t)}{h}$$

where  $p(x, y, z, t)$  is the fluid pressure. This approximation is obviously only reasonable if  $h$  is “small”. In one particular case he took  $h = 10^{-12}$  m which is smaller than the molecular length scale. In the light of the continuum hypothesis discuss whether this is a reasonable thing to do?

- (c) Non-dimensionalise the stress tensor as in part 6(a) and show that  $T_{ij} \approx -p\delta_{ij}$  for a thin film flow. What consequences does this have for lubricating films?

- (d) A two dimensional irrotational flow occupies the half-space  $y < 0$  and is given by the velocity potential  $\phi = \exp(ky) \sin(kx)$  ( $k > 0$ ). Calculate the velocity field. Show that the flow is incompressible and deduce that  $\phi$  must satisfy Laplace's equation  $\nabla^2 \phi = 0$ .

Calculate the stream function  $\psi(x, y)$  such that  $u = \frac{\partial \psi}{\partial y}$ ,  $v = -\frac{\partial \psi}{\partial x}$ .

- (e) For the 2D flow field  $\mathbf{u} = (\alpha x, -\alpha y)$ , show by computing the line integral that the circulation along the circle  $x^2 + y^2 = 1$  is zero.

Verify that his flow is incompressible and irrotational. Use the latter fact and Stokes' theorem to verify that the circulation in the first part of the question must be zero.

- (f) Incompressible viscous fluid of kinematic viscosity  $\nu$  lies at rest in the region  $0 < y < \infty$ . At  $t = 0$  the rigid boundary at  $y = 0$  is suddenly set into motion in the  $x$ -direction with constant speed  $U$ .

- (i) Show that a parallel flow of the form  $\mathbf{u} = u(y, t)\mathbf{i}$  develops and is governed by the equation

$$\frac{\partial u}{\partial t} = \nu \frac{\partial^2 u}{\partial y^2}.$$

- (ii) State the initial and boundary conditions for  $u(y, t)$ .

- (iii) Using a Laplace transform on the time variable, or otherwise, show that

$$u(y, t) = U \left( 1 - \operatorname{erf} \left( \frac{y}{2\sqrt{\nu t}} \right) \right).$$

You may use the following results:

$$\mathbf{L}[df/dt] = s\bar{f}(s) - f(0); \quad \mathbf{L} \left[ 1 - \operatorname{erf} \left( \frac{a}{2\sqrt{t}} \right) \right] = \frac{\exp(-a\sqrt{s})}{s}.$$

- (g) Find an approximate solution using matched asymptotic expansions to the singularly perturbed ordinary differential equation problem:

$$\epsilon \frac{d^2 u}{dy^2} + 2 \frac{du}{dy} + u = 0, \quad u(0) = 0, u(1) = 1, \epsilon \ll 1.$$

(Hint: Use  $y = \epsilon Y$  as an "inner" rescaling.)

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## Useful equations

Navier-Stokes equation:

$$\frac{D\mathbf{u}}{Dt} \left( = \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right) = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{u} + \mathbf{g}; \quad (\nu = \mu/\rho)$$

Navier-Stokes in index notation

$$\frac{Du_i}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_j \partial x_j} + g_i \quad (\text{summation convention})$$

Navier-Stokes in component form:

$$\begin{aligned} \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} &= -\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) + g_x \\ \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} &= -\frac{1}{\rho} \frac{\partial p}{\partial y} + \nu \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) + g_y \\ \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} &= -\frac{1}{\rho} \frac{\partial p}{\partial z} + \nu \left( \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right) + g_z \\ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} &= 0 \quad (\text{incompressibility}) \end{aligned}$$

Euler equations: put  $\nu = 0$  in the Navier-Stokes equations.

Cauchy's equation of motion:

$$\rho \frac{Du_i}{Dt} = \frac{\partial T_{ij}}{\partial x_j} + \rho g_i$$

Constitutive equation for a Newtonian Fluid:

$$T_{ij} = -p\delta_{ij} + \mu \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad (i, j = 1, 2, 3)$$

## Useful parameters

Reynolds number  $R = \rho UL/\mu \equiv UL/\nu$ .

Air:  $\nu = 15 \cdot 10^{-6} \text{m}^2 \text{s}^{-1}$ ;  $\rho = 1.205 \text{Kg m}^{-3}$ ; ( $\nu = \mu/\rho$ )

## Useful results

$$(\mathbf{u} \cdot \nabla) \mathbf{u} \equiv (\nabla \times \mathbf{u}) \times \mathbf{u} + \nabla(\mathbf{u}^2/2), \quad \mathbf{u}^2 \equiv \mathbf{u} \cdot \mathbf{u} \equiv |\mathbf{u}|^2$$

$$\nabla \times (\mathbf{a} \times \mathbf{b}) \equiv (\mathbf{b} \cdot \nabla) \mathbf{a} - (\mathbf{a} \cdot \nabla) \mathbf{b} + \mathbf{a} \nabla \cdot \mathbf{b} - \mathbf{b} \nabla \cdot \mathbf{a}$$

$$\frac{Df}{Dt} \equiv \frac{\partial f}{\partial t} + \mathbf{u} \cdot (\nabla f)$$



**Tensor divergence theorem**

$$\iint_S T_{ij} n_j dS = \iiint_V \frac{\partial T_{ij}}{\partial x_j} dV.$$

**Error function**

$$\operatorname{erf}(x) \equiv \frac{2}{\sqrt{\pi}} \int_0^x e^{-s^2} ds, \quad \operatorname{erf}(0) = 0, \quad \operatorname{erf}(\infty) = 1.$$